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Thermodynamic Properties of Isopentane

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The thermodynamic properties, entropy, enthalpy, and specific volume, were calculated for isopentane using experiemntal data from the literature. The calculations were based on rigorous thermodynamic equations using the Benedict-Webb-Rubin (*B-W-R*) equation of state to give analytical expressions for the entropy, enthalpy, and volume. The results are presented in the form of tables and graphs from 1 to 60 atm. and 50° to 600° F. for the superheated vapor, and from 0° F. to the critical point for the saturated liquid and vapor.

LXPERIMENTAL thermodynamic data for isopentane have been published in the literature. However, the derived thermodynamic functions, enthalpy and entropy, have not been published previously. The present paper gives the calculated values of the enthalpy, entropy, and specific volume for the superheated vapor from 1 to 60 atm. and from 50° to 600° F., and for the saturated liquid and vapor from 0° F. to the critical point.

The calculations were based upon rigorous thermodynamic relations using the Benedict-Webb-Rubin (B-W-R)equation of state,

$$P = \frac{RT}{V} + \frac{B_0 RT - A_0 - C_0 / T^2}{V^2} + \frac{bRT - a}{V^3} + \frac{a\alpha}{V^6} + \frac{c}{T^2 V^3} \left[\left(1 + \frac{\gamma}{V^2} \right) e^{-\gamma/V^3} \right]$$

A new set of constants for the B-W-R equation of state were calculated using selected experimental data from the literature.

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DATA AND METHODS OF CORRELATION

The literature was thoroughly reviewed to find the best data on which to base the calculations. The following sections show the sources of all data used.

P.V.T Date. The *P-V-T* behavior of isopentane has been studied by Young (15), Silberberg, McKetta, and Kobe (11), Vohra and Kobe (12), and Isaac, Li, and Canjar (4). The findings of Silberberg, McKetta, and Kobe and of Vohra and Kobe agree very well, within 0.2% maximum difference, even though completely different types of experimental apparatus and techniques were used in the two investigations. However, the results of Isaac, Li, and Canjar, and of Young deviated widely from the other two and did not agree with each other. Therefore, the data of Silberberg, McKetta, and Kobe (11) and Vohra and Kobe (12) were used in the present work.

Constants for the \vec{B} -W-R equation have been determined by Benedict, Webb, and Rubin (2) based on the data of Young. Since Young's data were thought to be inferior to the data used in this work, new constants were calculated using a least squares method described by Brough (3). The constants calculated in this manner are shown in Table I.

The data on which the constants are based include pressures up to 60 atm. There are only five useful data points between 60 and 200 atm. Checks of the B-W-R

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Table I. Constants for the B-W-R Equation of
State for Isopentane
Units correspond to pressure in atm., temperature in ° R.
and volume in cu. ft. per pound)

Constant	Values
$B_0 \times 10^3$	-8.83680
$A_0 imes 10^1$	1.76210
$C_0 \times 10^{-5}$	3.36705
$b \times 10^{3}$	-1.12055
$a \times 10^2$	-2.86318
$c \times 10^{-3}$	3.32652
$\alpha \times 10^8$	1.29180
$\gamma \times 10^3$	7.00339
$R \times 10^2$	1.01216

equation using the new set of constants showed that deviations become as large as 20% as pressure increases over this range. The constants fitted in this manner probably make the *B*-*W*-*R* equation unsuitable for extrapolation beyond 60 atm. Using the new set of constants, the standard deviation of the compressibility factor, *z*, is 2.3×10^{-3} based on the 138 available data points below 60 atm., and the maximum deviation is 3.4% at 59.46 atm. and 392° F. The standard deviation of *z* using the same data and the constants determined by Benedict, Webb, and Rubin (2) is 5.6×10^{-3} .

Vapor Pressure Data. The vapor pressure data of Willingham, Taylor, Pignocoo, and Rossini (14) and of Schumann, Aston, and Sagenkahan (10), as interpolated and tabulated in the API Research Project 44 (9), were used in the temperature range 0° to 120° F. The data of Silberberg (11) were used for the temperature interval 122° to 347° F. The critical constants of isopentane have been measured by Vohra and Kobe (12), Young (16), Pawlewski (5), and Altschul (1). A comparison of their results is shown in Table II.

The critical constants of Vohra and Kobe were used in the present work. The reasons are that the data of Vohra and Kobe are the most recent and their extensive P-V-T data

Source	t_c , ° C.	P_c , Atm.	ρ_c , G./Cc.
Vohra (12) Young (16) Pawlewski (5) Altschul (1)	$\begin{array}{l} 187.8 \pm 0.05 \\ 187.8 \\ 194.8 \\ 187.1 \end{array}$	33.66 ± 0.05 32.9 33.3	$\begin{array}{c} 0.236 \pm \ 0.005 \\ 0.2343 \end{array}$

Table III. Constants for the Modified Antoine Equation

130° Constant 0° to 120° F. 370.78		Temperature	e Range
A 9.7079 AA	onstant	0° to 120° F.	130° to 370.1° F
1 0.1910 4.4		3.7978	4.4466
3×10^{-3} 1.6707 2.40	$\times 10^{-3}$	1.6707	2.4654

near the critical point were used in the evaluation of the constants of the B-W-R equation of state. Also, the critical constants of Vohra and Kobe agree well with the older determinations by Young and Altschul.

A modified Antoine equation,

$$\log P = A - \frac{B}{t+D} + \frac{C}{(t+D)^2}$$

was used both to interpolate the vapor pressure data of Silberberg and to calculate latent heats via the Clapeyron equation. To refine further this correlation, the best constants, based on the least squares method, were calculated for each temperature range covered by the two sources of data (Table III). The consistency between these two sets of constants, and the data they represent, at the junction of the two temperature ranges was checked both by plotting log Pvs. 1/(t + D) and by comparing the values of the first derivative of P with respect to t calculated with each set of constants at 120° and 130° F. Both methods



Figure 1. Pressure-enthalpy diagram for isopentane

Table IV. Thermodynamic Properties of Saturated Isopentane

	(Datum: H	and $S = 0$ for	r ideal gas at 0° R	. and 1 p.s.i.a.)
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Temp	Pres	ssure	Volume, Cu. Ft./Lb.		Enthalpy, B.T.U./Lb.		Entropy, B.T.U./Lb., ° R.	
° F.	P.s.i.a.	Atm.	Liquid	Vapor	Liquid	Vapor	Liquid	Vapor
 F. 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 	P.s.i.a. 2.18 2.87 3.73 4.78 6.05 7.59 9.42 11.57 14.12 17.06 20.46 24.35 28.79 33.86 39.46 45.77 52.84	Atm. 0.15 0.20 0.25 0.33 0.41 0.52 0.64 0.79 0.96 1.16 1.39 1.66 1.96 2.30 2.69 3.11 3.60 4.12	Liquid 0.02440 0.02461 0.02501 0.02522 0.02544 0.02567 0.02590 0.02614 0.02614 0.02639 0.02664 0.02691 0.02718 0.02718 0.02747 0.02776 0.02807 0.02838 0.02837	Vapor 31.00 23.99 18.79 14.92 11.98 9.69 7.92 6.53 5.43 4.54 3.83 3.25 2.77 2.40 2.06 1.78 1.55 1.25	Liquid -58.8 -53.8 -48.7 -43.5 -38.3 -33.0 -27.6 -22.1 -16.6 -11.1 -5.5 0.2 5.9 11.6 17.4 23.2 29.0	Vapor 102.9 106.2 109.6 113.0 116.5 120.0 123.5 127.1 130.7 134.3 137.9 141.5 145.1 145.1 145.1 145.2 5 156.1 159.8	Liquid 0.7807 0.7918 0.8023 0.8131 0.8236 0.8340 0.8445 0.8549 0.8651 0.8751 0.8852 0.8954 0.9051 0.9151 0.9247 0.9344 0.9437	Vapor 1.1325 1.1325 1.1323 1.1327 1.1334 1.1342 1.1353 1.1366 1.1380 1.1396 1.1414 1.1434 1.1454 1.1478 1.1500 1.1524 1.1548 1.1548
$170 \\ 180 \\ 190 \\ 200 \\ 210 \\ 220 \\ 230 \\ 240 \\ 250 \\ 260 \\ 270 \\ 280 \\ 290 \\ 300 \\ 310 \\ 320 \\ 330 \\ 340 \\ 350 \\ 360 \\ 370.1$	$\begin{array}{c} 60.72\\ 69.49\\ 79.20\\ 89.92\\ 101.70\\ 114.70\\ 128.80\\ 144.2\\ 160.9\\ 179.1\\ 198.7\\ 219.9\\ 242.7\\ 267.2\\ 293.4\\ 321.4\\ 351.4\\ 351.4\\ 351.4\\ 351.4\\ 453.0\\ 494.7\\ \end{array}$	$\begin{array}{c} 4.13\\ 4.73\\ 5.39\\ 6.12\\ 6.92\\ 7.80\\ 8.76\\ 9.81\\ 10.95\\ 12.19\\ 13.52\\ 14.96\\ 16.51\\ 18.18\\ 19.96\\ 21.87\\ 23.91\\ 26.08\\ 28.38\\ 30.82\\ 33.66\end{array}$	0.02870 0.02905 0.02942 0.02942 0.03025 0.03115 0.03115 0.03221 0.03281 0.03281 0.03281 0.03421 0.03498 0.03584 0.03684 0.03806 0.03960 0.04129 0.04375 0.04762 0.06790	$\begin{array}{c} 1.35\\ 1.19\\ 1.04\\ 0.917\\ 0.810\\ 0.720\\ 0.636\\ 0.565\\ 0.500\\ 0.442\\ 0.390\\ 0.346\\ 0.307\\ 0.276\\ 0.249\\ 0.222\\ 0.195\\ 0.168\\ 0.138\\ 0.1055\\ 0.0679\end{array}$	$\begin{array}{c} 34.9\\ 40.9\\ 46.9\\ 53.0\\ 59.1\\ 65.3\\ 71.7\\ 78.6\\ 85.9\\ 93.3\\ 101.7\\ 108.2\\ 115.7\\ 123.5\\ 131.6\\ 140.0\\ 148.8\\ 158.3\\ 169.0\\ 181.7\\ 202.9 \end{array}$	$\begin{array}{c} 163.5\\ 167.2\\ 170.9\\ 174.7\\ 178.4\\ 182.1\\ 185.7\\ 189.3\\ 192.8\\ 196.2\\ 199.5\\ 202.8\\ 206.1\\ 209.5\\ 212.9\\ 216.1\\ 209.5\\ 220.1\\ 219.7\\ 216.1\\ 202.9 \end{array}$	0.9531 0.9626 0.9717 0.9809 0.9900 0.9992 1.0083 1.0182 1.0285 1.0285 1.0285 1.0387 1.0488 1.0589 1.0688 1.0792 1.0898 1.1003 1.1114 1.1232 1.1362 1.1512 1.1763	1.1573 1.1600 1.1626 1.1654 1.1681 1.1710 1.1736 1.1764 1.1791 1.1817 1.1842 1.1842 1.1842 1.1842 1.1894 1.1924 1.1924 1.1979 1.1971 1.2005 1.1988 1.1932 1.1763

demonstrated good consistency of the vapor pressure data from the two sources.

Saturation Volumes. The saturated liquid volumes were taken from the International Critical Tables (13) and covered the range from 86° F. to the critical point. From 0° to 80° F., the liquid volumes at 1 atm. were taken from API Research Project 44 (8). Changing the pressure from 1 atm. to the saturation pressure would have a negligible effect on the liquid volume in this range.

The saturated vapor volumes were taken from the work of Silberberg (11) for the temperature range from 130° F. to the critical point. Below 130° F., the *B-W-R* equation was employed using the vapor pressure data calculated from the modified Antoine equation.

Ideal Gas State Properties. The ideal gas state properties for isopentane were taken from API Research Project 44 (6, 7). Graphical interpolation of the enthalpy, H° , and the entropy, S° , was carried out to find the values at the proper intervals for the present work. The datum state was chosen to be identical to that used in the API Research Project 44—namely, the ideal gas state at absolute zero temperature and 1 p.s.i.a.

METHODS OF CALCULATION

The equations used to calculate the enthalpy and the entropy of isopentane in the superheated region and for the saturated vapor were formulated by substituting the B-W-R equation of state into rigorous thermodynamic relations between the properties in the real state and in the ideal gas state at the same temperature. The integrated expressions which were used are:

$$H = H^{\circ} + PV - RT - \frac{A_0}{V} - \frac{a}{2V^2} + \frac{a\alpha}{5V^2} - \frac{3}{T^2} \left[\frac{C_0}{V} - \frac{c}{\gamma} + \left(\frac{c}{\gamma} + \frac{c}{2V^2} \right) e^{-\gamma/V^2} \right]$$
$$S = S_{1\text{ p.s.i.a.}}^{\circ} + R \left[\ln \frac{V}{RT} - \frac{B_0}{V} - \frac{b}{2V^2} \right] - \frac{b}{2V^2}$$

$$\frac{2}{T^3} \left[\frac{C_0}{V} - \frac{c}{\gamma} + \left(\frac{c}{2V^2} \right) e^{-\gamma/V^2} \right]$$

In the latter equation, the R in the term, $\ln(V/RT)$, must be used in units of (cu. ft.-p.s.i.a.)/(pound_m, °R.) rather than (cu. ft.-atm.)/(pound_m, °R.), since this term arises from the $\ln V/V_{1p.s.i.a.}^{\circ}$ term of the integration, by replacing $V_{1p.s.i.a.}^{\circ}$ with (RT/P) where P = 1 p.s.i.a. The latent heats of vaporization were determined by

The latent heats of vaporization were determined by differentiating the modified Antoine equation and substituting it into the Clapeyron equation to give:

$$\Delta H_{s} = \frac{6.265 PT}{(t+D)^{2}} \left(B - \frac{2C}{t+D} \right) (V_{s} - V_{l})$$

From the smoothed latent heats and saturated vapor properties, the enthalpy and entropy of the saturated liquid were readily calculated. All of the computations were performed on a digital computer.

Table V. Thermodynamic Properties of Superheated Isopentane

 $\begin{array}{l} (\text{Datum: } H \text{ and } S = 0 \text{ for ideal gas at } 0^{\circ} \text{ R. and } 1 \text{ p.s.i.a.}) \\ (\text{Units: } H, \text{B.t.u./lb.; } S, \text{B.t.u./lb. }^{\circ} \text{ R.; } V, \text{cu. ft./lb.}) \end{array}$

P	Pron-					Temperat	ture, ° F.				
Atm.	erty	100	120	140	160	180	200	220	240	260	280
1 2 3	H S V H S V H S V H S	138.86 1.1518 5.4310	147.29 1.1667 5.6558	$155.60 \\ 1.1815 \\ 5.8772 \\ 153.95 \\ 1.1599 \\ 2.8334$	$\begin{array}{c} 164.87\\ 1.1961\\ 6.0967\\ 163.03\\ 1.1748\\ 2.9527\\ 161.06\\ 1.1613\\ 1.1613\\ \end{array}$	$174.02 \\ 1.2106 \\ 6.3136 \\ 172.35 \\ 1.1896 \\ 3.0696 \\ 170.58 \\ 1.1765 \\ 1.1765 \\ 1.058 \\ 1.1765 \\ 1.$	$183.46 \\ 1.2251 \\ 6.5288 \\ 181.94 \\ 1.2044 \\ 3.1843 \\ 180.34 \\ 1.1914 \\ 1.1914 \\ 1.9040 \\ 1$	$193.07 \\ 1.2394 \\ 6.7426 \\ 191.68 \\ 1.2189 \\ 3.2974 \\ 190.23 \\ 1.2062 \\ 1$	202.88 1.2536 6.9552 201.60 1.2333 3.4094 200.27 1.2207	$213.07 \\ 1.2681 \\ 7.1667 \\ 211.90 \\ 1.2479 \\ 3.5199 \\ 210.68 \\ 1.2355 \\ 1$	$\begin{array}{c} 223.36 \\ 1.2825 \\ 7.3773 \\ 222.27 \\ 1.2624 \\ 3.6295 \\ 221.15 \\ 1.2502 \\ 1.2502 \end{array}$
5 10	V H S V H S				1.9008	1.9851	2.0669 176.86 1.1735 1.1679	$2.1471 \\187.11 \\1.1887 \\1.2227$	2.2256 197.45 1.2037 1.2756	$\begin{array}{c} 2.3030\\ 208.11\\ 1.2189\\ 1.3268\\ 200.58\\ 1.1919\end{array}$	$2.3790 \\218.80 \\1.2338 \\1.3768 \\212.08 \\1.2080$
	V									0.5844	0.6171
Ρ,	Prop					Tempera	ture, ° F.				
Atm.	erty	300	320	340	360	380	400	450	500	550	600
1	H S V	233.93 1.2968 7.5871	$244.70 \\ 1.3110 \\ 7.7963$	$255.66 \\ 1.3251 \\ 8.0048$	266.91 1.3389 8 2122	278.37 1.3525 8.4197	290.01 1.3659 8.6269	320.11 1.3992 9.1431	351.09 1.4330 9.6567	383.35 1.4661 10.169	417.01 1.4984 10.681
2	H S V	232.92 1.2768 3.7382	243.76 1.2911 3.8461	254.79 1.3053 3.9535	266.10 1.3191 4.0599	277.60 1.3328 4 1662	289.29 1.3463 4 2720	319.49 1.3797 4 5350	350.55 1.4136 4 7961	382.88 1.4467 5.0555	416.58 1.4790 5.3138
3	H S V	$231.89 \\ 1.2647 \\ 2.4542$	$242.80 \\ 1.2790 \\ 2.5286$	253.89 1.2934 2.6023	265.27 1.3073 2.6754	276.82 1.3210 2.7480	$288.56 \\ 1.3345 \\ 2.8202$	318.87 1.3681 2.9988	350.00 1.4020 3.1753	382.40 1.4353 3.3507	$\begin{array}{r} 416.16 \\ 1.4676 \\ 3.5247 \end{array}$
5	H S V	$229.73 \\ 1.2486 \\ 1.4255$	$240.81 \\ 1.2632 \\ 1.4733$	$252.05 \\ 1.2777 \\ 1.5205$	$263.55 \\ 1.2917 \\ 1.5669$	$275.22 \\ 1.3056 \\ 1.6127$	$287.07 \\ 1.3193 \\ 1.6580$	317.59 1.3530 1.7693	$348.90 \\ 1.3872 \\ 1.8787$	$381.44 \\ 1.4206 \\ 1.9867$	$\begin{array}{r} 415.31 \\ 1.4530 \\ 2.0933 \end{array}$
10	H S V	223.67 1.2237 0.6479	$235.31 \\ 1.2389 \\ 0.6772$	$247.02 \\ 1.2540 \\ 0.7052$	$258.93 \\ 1.2686 \\ 0.7323$	$270.95 \\ 1.2829 \\ 0.7586$	$383.11 \\ 1.2969 \\ 0.7843$	$314.26 \\ 1.3314 \\ 0.8461$	$346.05 \\ 1.3661 \\ 0.9054$	378.96 1.3998 0.9630	$\begin{array}{r} 413.13 \\ 1.4326 \\ 1.0193 \end{array}$
20	H S V		219.89 1.2044 0.2594	$233.87 \\ 1.2223 \\ 0.2840$	247.40 1.2389 0.3051	260.67 1.2547 0.3242	273.83 1.2699 0.3417	306.81 1.3065 0.3812	339.87 1.3425 0.4169	373.70 1.3772 0.4501	408.57 1.4106 0.4817
30	H S V				$225.79 \\ 1.2054 \\ 0.1359$	245.17 1.2285 0.1655	$261.19 \\ 1.2472 \\ 0.1854 \\ 0.27 00 \\ 0.00 $	297.88 1.2879 0.2226	332.88 1.3260 0.2522	367.97 1.3620 0.2782	403.73 1.3963 0.3019
40	н S V u					194.23 1.1647 0.0500	237.00 1.2147 0.0898	$ \begin{array}{r} 286.51 \\ 1.2701 \\ 0.1398 \\ 271.94 \end{array} $	324.88 1.3118 0.1686 315.82	301.73 1.3496 0.1917 255.01	398.60 1.3850 0.2119
50	S V H					1.1538 0.0431 182.90	$ \begin{array}{r} 209.89 \\ 1.1813 \\ 0.0499 \\ 203.76 \\ \end{array} $	1.2508 0.0891 258 17	$ \begin{array}{r} 313.82 \\ 1.2984 \\ 0.1183 \\ 306 41 \end{array} $	1.3386 0.1399 348 11	1.3752 0.1580 387 79
60	S V H					1.1483 0.0401 179.08	$ 1.1726 \\ 0.0440 \\ 198.50 $	1.2334 0.0624 246.08	1.2857 0.0868 292 19	1.3284 0.1064 336.01	1.3665 0.1228 377 77
80	S V H					1.1413 0.0367 176 93	1.1639 0.0389 195.90	1.2170 0.0463 241.70	1.2670 0.0572 285 55	1.3118 0.0699 328 38	1.3519 0.0820 370.40
100	S V H					1.1364 0.0346 174.33	1.1585 0.0362 193.00	1.2096 0.0409 237.77	$\begin{array}{r} 200.03\\ 1.2572\\ 0.0469\\ 280.25\end{array}$	$\begin{array}{r} 1.3010 \\ 0.0541 \\ 321.66 \end{array}$	1.3413 0.0620 362.68
150	S V H					1.1280 0.0314 173 49	1.1498 0.0324 192.15	1.1997 0.0350 236 90	1.2458 0.0377 279 29	1.2882 0.0406 320 56	$ 1.3275 \\ 0.0437 \\ 361 40 $
200	S V					1.1221 0.0293	1.1439 0.0301	1.1937 0.0319	1.2397 0.0337	1.2820 0.0355	1.3212 0.0373

The results are presented in Tables IV and V and in Figure 1. It should be remembered that the B-W-R equation gave a poor fit to the P-V-T points above 60 atm., so the tabulated and graphed results are probably not accurate much above 60 atm.

The internal consistency of the results was checked by using the relations:

$$\left(\frac{\partial \ln P}{\mathrm{d}H}\right)_{s} = \frac{1}{PV}$$
$$\left(\frac{\partial H}{\partial S}\right)_{p} = T$$

The slopes measured on the appropriate graphs were compared with the quantities on the right hand side of the above equations. Agreement was within 0.4% at the 10 points that were checked. The error introduced into the entropy and enthalpy owing to the use of the B-W-Requation of state is estimated at about 1% in the enthalpy and 0.5% in the entropy. This error was estimated by observing the variation in H and S as the B-W-R equation was made to fit the experimental data more and more closely.

NOMENCLATURE

- A,B,C,D = constants in the modified Antoine equation $A_0, B_0, C_0,$ a,b,c,α,γ = constants in the Benedict-Webb-Rubin equation
 - of state H =
 - enthalpy of real gas state, B.t.u./lb. H° =
 - enthalpy of ideal gas state, B.t.u./lb.
 - ΔH_v = latent heat of vaporization, B.t.u./lb.
 - P = absolute pressure, atm.
 - P_c = critical pressure, atm.
 - R = gas constant for isopentane

- S= entropy of real gas state, B.t.u./lb., ° R.
- S° = entropy of ideal gas state, B.t.u./lb., °R.
- $t = \text{temperature}, \circ F.$ \dot{T}
 - = absolute temperature, ° R., = t ° F. + 459.688
- V =specific vapor volume, cu. ft./lb.
- $V_{g} = V_{l}$ specific volume of saturated vapor, cu. ft./lb. =
- specific volume of saturated liquid, cu. ft./lb. =
- z =compressibility factor, pV/RT

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Compressibility Factors for Helium-Nitrogen Mixtures

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> Experimental compressibility factors for the helium-nitrogen system from -140° to 0° C. up to 500 atm. were determined by the Burnett method. A total of 1186 compressibility factors for the two pure components and six mixtures are reported. Derived thermodynamic properties of this system are compared with recent calorimetric determinations.

m THIS PAPER presents compressibility factors for the helium-nitrogen system from 0° to 140° C. at pressures to 500 atm. Compressibility data for this system have been reported by a number of previous investigators, but no data in the present temperature range have been published. Pfefferle, Goff, and Miller (13), Kramer and Miller (6), and

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Witonsky and Miller (17) have published data on the helium-nitrogen system at temperatures from 30° to 475° C. and at pressures to 100 atm. Other data have been collected by Ku (7) at 38.48° and 100°C. up to 295 atm. Miller, Brandt, and Stroud (10) report compressibility factors at 70° F. up to 4000 p.s.i.a. Such an abundance of data has been published for pure helium and pure nitrogen that it will be left to the writers of monographs to review these data. The present authors collected data for the pure components